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.24 MAY 1948

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE

No. 1438

EFFECT OF SIMULATED SERVICE CONDITIONS ON PLASTICS

DURING ACCELERATED AND 2-YEAR

WEATHERING TESTS

By W. A. Crouse, D. C. Caudill, and F. W. Reinhart

National Bureau of Standards

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SUMMARY

The effects of outdoor weathering for 2 years and of an accelerated weathering test on the weight, dimensional stability, and flexural properties of selected reinforced plastics were investigated. The results of all tests, both in this report and the previous report (NACA TN No. 1240), indicate that none of the laboratory aging tests correlated with outdoor weathering with respect to all properties and all materials.

INTRODUCTION

This report supplements information given in a previous report on this same subject (reference 1). The results of a 2-year outdoor weathering test and an accelerated weathering test (Method 6023, reference 2) on the weight, dimensional stability, and flexural properties of selected reinforced plastics are presented.

This investigation, conducted at the National Bureau of Standards, was sponsored by and conducted with the financial assistance of the National Advisory Committee for Aeronautics.

MATERIALS AND TEST PROCEDURES

The materials tested were the same as those used in the tests previously reported in reference 1. A description of the materials is given in table I, which has been reproduced from reference 1 for convenience. The dimensions of the specimens were also the same as those described in reference 1.

The 2-year outdoor weathering test was a continuation of the 1-year test previously reported (reference 1).

The accelerated weathering test was made in accordance with Method No. 6023 of Federal Specification L-P-406a (reference 2). This test involves exposure to cycles of soaking, freezing, drying, and radiation rich in ultraviolet light. The conditions used in this test are as follows:

- 24 hours at 100° F (38° C) over water 4 hours at -70° F (-57° C) 16 hours at 160° F (71° C)
- 4 hours of exposure to ultraviolet radiation

In (a) the condition was obtained by suspending the specimens individually over water in 8-ounce bottles. In (b) and (c) the low and high temperatures were attained by placing the specimens in a lowtemperature test cabinet and in a circulating-air oven, respectively. In (d) the source of ultraviolet radiation was an S-1 bulb in a sunlamp, as specified in Method No. 6021 of reference 2. During this part of the cycle the specimens were turned end for end every 2 hours to obtain more uniform exposure to the radiation over the entire length. The bolts and nuts above the disk were arranged so as to-be suitable for holding the 1- by 3-inch specimens.

The weight and dimensions of one set of specimens were measured within 10 minutes after the conclusion of 1, 3, 5, and 10 cycles. The flexural properties were determined on other sets at the end of 5 and 10 cycles, respectively, after conditioning at 77° F and 50-percent relative humidity for 48 hours.

RESULTS AND DISCUSSION

Weight and Dimensional Changes

The percentage changes in weight, length and width, and thickness of the materials on exposure to the 2-year outdoor weathering and accelerated weathering tests are shown in table II. In most instances the percentage changes in weight, length, width, and thickness decreased. Of those showing increases, most were observed in thickness.

Comparing the accelerated service tests generally, test IV caused the greatest changes followed by accelerated weathering test 6023; it is to be noted, however, that the effects of accelerated tests are different from the outdoor weathering test as shown by the differences in the rankings (table III) for the outdoor and for the accelerated service tests.

The relative weight and dimensional stability of the various materials are shown in table III. The results of aging tests shown in table V of reference 1 are incorporated into this table for comparison. The rating method is the same as used in reference 1.

Changes in Flexural Properties

The percentage changes in flexural strength, flexural modulus of elasticity, and maximum deflection in flexure of the materials on exposure to the 2-year outdoor weathering and accelerated weathering tests are shown in table IV.

Considering the tests shown in table TV of reference 1 and table TV of the present report, the 10-cycle accelerated service test TV gives percentage changes in flexural strength of approximately the same order of magnitude as the 2-year outdoor weathering and is the most severe of the aging procedures with respect to changes in flexural strength. However, the rankings of different materials for the outdoor weathering and accelerated weathering test TV are not in concordance.

The relative retention of flexural strength by the various materials is shown in table III. The aging tests shown in table V of reference l are incorporated into this table for comparison. The rating method is the same as used in reference 1.

Correlation of Laboratory Aging Tests

with Outdoor Weathering

Correlation coefficients of rank were obtained by comparing the rankings of the plastics for the accelerated weathering tests with the rankings for the outdoor weathering tests. No accelerated weathering tests correlated with the outdoor weathering tests sufficiently well to be regarded in any way as a useful substitute. It is worth noting that the five accelerated service tests show concordance among themselves to a statistically significant extent, though they do not reproduce the ranking of the outdoor weathering tests.

CONCLUSION

A comparison of the degree of correlation of the results obtained in the various laboratory aging procedures with those observed in the 1- and 2-year exposure tests out of doors, confirms the previous conclusion that none of the laboratory tests give results with all the materials and for all the properties which correlate with the results of outdoor weathering.

National Bureau of Standards
Washington, D. C., April 16, 1947

REFERENCES

- 1. Crouse, W. A., Caudill, D. C., and Reinhart F. W.: Effect-of Simulated Service Conditions on Plastics. NACA TN No. 1240, 1947.
- 2. Federal Specification L-P-406a: Plastics Organic; General Specifications, Test Methods; Jan. 24, 1944. Government Printing Office, Washington 25, D. C.

TARE I. - DESCRIPTION OF MATERIALS

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From reference il

												
		(witn)	ю. 						Gradual	&	% 	ଷ
Tine	Curing (min)		1 3						2 hours at 158° F 10 hours at 158-239° F	28	ξ.	R .
dons	Curing temperature Initial Maximum (OF)		88						682	9£	ă,	3 1 0
Molding conditions	Curing te	Initial (OF)	8						1,78	<u>.</u>	<u>.</u>	
Mold	Pressure (lb/sq in.)		8100	0 6	ଧି				2-5	1800	1620	1800
	9	no. or					7	t-	9	t	91	n
	Ply arrengement			Parallel	Crossed		Crossed		Стовней	Grossod	Parallel	Parellol
sement	Thread count	Warp Filling	ı	:	;	ſ.	1,7	84	SK	.⊋i	8	91
Reinforcement	Threa	Yerp]	l	1	· ;	1	87	٤	%	ደ	8	87
1	⊕đ.£ī		Macarated cotton fabric	Paper	Paper	Lignin paper	Glass febrio, plain weave ECC-11-162	Cotton fabric (muslin), twill weave	Ootton fabrio (enemeled duok), plain weave	Cotton fabrio, plain weave, 10 or/eq yd	Cotton fahrio, plain weave, 3.7 oz/sq yd	Asbestos fabrio, plain wave, 18 cz/są yd
r]	Content by weight (percent)								62-63	84	9K-94	14
Regin	Type		Balcelite EM-199			Ligain	Marco MR-1A	Marco MR-1A	Allymer CR39	Bakelite No. 1112	Balcalite BV-1112	Bakelite No. 2427
	Density	(8/cn cm)	1.37	1.43	1.43	1,38	1.70	1.27	1.37	1.36	461	1.3
	Average thickness	(т.)	0.121	ह्यः	कृतः	921.	911.	ır.	.145	81.	Si.	6 41.
	Manufacturer		Bakelite Corp.	Consolidated Water Power and Paper Go.	Consolidated Water Power and Paper Co.	Formica Insulation Go.	Swedlow Aeroplastics Corp.	Swedlow Aeroplastics Corp.	Pittsburgh Plate Glass Co., Columbia Chemical Division	Synthene Corp.	Synthene Corp.	Egrithane Corp.
	Type of laminatel		Macerated-cotton-fahric Bakelite Corp. phenolic molding compound	Eigh-strength paper, phenolic	Eigh-strength paper, phenolic	Lignin paper	Glass-fabric, unsaburted polyester	Mualin-cotton-fabrio, unsaturated polyester	Enameled-duck cotton- fabric, unsaturated polyester	Grade C phenolic	Grade I phemolio	Grade AA phenalic
	RES natorial designation		T	Ħ	ຜ	ជ	ri A	g .	d	ri	Ę.	퇴

Asterial Al was obtained in the form of sheets prepared from a molding compound; all of the other materials were leminated sheet products.

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TABLE II. - CHANGES IN WEIGHT AND DIMENSIONS OF PLASTICS DURING OUTDOOR AND ACCELERATED WEATHERING TESTS

Material desig-	Change during outdoor weathering test,	Changes during accelerated weathering test									
nation	2 years (percent) (a)	l cycle (percent)	3 cycles (percent)	5 cycles (percent)	10 cycles (percent)						
Weight											
Al Blc Bld Cl Dl El Fl El Tl Jl Kl	-1.05 1.63 1.68 1.52 .30 49 22 20 79 92	-2.26 73 79 85 -1.34 -1.50 -1.27 -1.70 -1.42 -1.22	-3.10 62 76 87 -1.70 43 -1.58 -2.25 -1.88 -1.36	-3.44 65 81 97 -1.88 47 -2.00 -1.69 -2.47 -2.12 -1.38	-3.98 76 98 -1.13 -2.10 56 -2.26 -1.93 -2.74 -2.42						
	Length and width										
Al BlC Bld Cl Dl El Hl Tl Jl Kl	-0.18 16 20 16 12 .02 22 18 12 11	-0.26 14 14 08 16 .00 20 19 16 14 07	-0.38 16 14 10 20 .00 24 26 22 20	-0.44 16 14 10 23 .00 28 26 27	-0.54 18 20 08 30 .00 36 38 15 30 13						
	Thickness										
Al Blo Bld Cl Dl El Fl Hl Jl	0.46 4.33 4.85 4.06 1.10 .39 1.17 .96 05 03	-0.04 .22 .27 .03 18 .28 19 .11 13 08 05	-0.04 •55 •43 •14 •11 •10 •08 •02 •24 •05 •13	0.08 .63 .71 .27 13 .10 14 .12 13 19 15	-0.35 .44 .41 02 41 19 -2.18 09 24 43 36						

^aWashington, D. C.; specimens facing south on racks inclined at 45°. NACA bhothod No. 6023, Federal Specification L-P-406a (reference 2). CSpecimens cut lengthwise. dSpecimens cut crosswise.

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TABLE III .- STABILITY RATINGS OF THE PLASTIC MATERIALS IN OUTDOOR MEATHERING,

ACCELERATED WEATHERING, AND ACCELERATED SERVICE TESTS

	r		•••				T							<u> </u>	<u> </u>	· <u> </u>
Material		Weathering Accelerated				Accelerated			Accelerated service test-							
designa- tion		tdoor	1 1	5021 (0)	1 .	lerated 6023 (d)		I		п		m		IA		▼
	l yr	2 Jr	120 hr	240 hr	5 cg	10 cy	5 cy	20 cy	5 cg	10 ch	5 cg	10 cy	5 cg	10 cy	5 cg	10 cy
Weight ^b											,					
AL BL ^f CI DL EL EL EL EL EL	8 9 11 10 1 2 5.5 3 7 5.5	8 10 11 9 3 4 2 1 5 7 6	11 2 4 3 9 1 6 7 10 8 5	11 3 4.5 10 1 6 7 8 8	11 2 3 4 7 1 8 6 10 9 5	11 2 3 7 1 8 6 10 9 5	11 3 4 5 2 8 7 10 96	11 3 4 6 2 7.5 10 9 5	15689134072	16789134052	111347268295	11 1.5 3 7 1.5 9 10 8 5	13218407965	12 1 38 4 10 7 9 6 5	11 2 4 5 7 1 6 9 10 8 3	134 57 16 9 19 8 2
	Terroth and reface 0											22				
AL M° CI DI FI FI FI FI FI FI FI FI FI F	2.5 7.5 10 7.5 1 9 11 5 2.5	8.5 6.5 10 6.5 1 18.5 1.5 3	9.5 3.5 3.5 1 7 9.5 12 5	10 3.5 2.5 3.5 1 7 8.5 11 6 5	15 4 37 1 9 1 8 6 2	11 5 6 2 7-5 1 9 10 4 7-5 3	12638149645	11 2 5 38 1 50 97 5	11 5 4 2.5 9 1 6 8 10 7	11 5 3 3 9 1 6 8 9 7 2	11 2.5 4.5 7 18 10 96 5	11 34 2 7 1 8 9,5 5 5	94.5 321108764.5	8 4 3 2 11 10 9 7 6 5	11 2.5 4 2.5 7 1 8 10 96 5	11 · 3.5 · 3.5 · 2 · 7 · 1 · 8.5 · 1 · 8.5 · 6 · 5 · 5 · 5 · 5 · 5 · 5 · 5 · 5 ·
			·			-		hickness	<u> </u>		<u></u>	<u> </u>				
AL SELECTION OF THE COLUMN OF	30 11 97 486 215	10 11 9 7 3 8 6 2 1 5	7 28.5 20 18.5 5 3 11	78 4 10 11 1 9 2 6 5 3	1 10 11 9 4.5 26 3 4.5 7	5 10 7.5 1 7.5 31 2.4 96	2.5 10 11 96 2.7 8 51	6.5 10 11 95 38 6.5 21	6 10 91 18 1 7 34 5 2	70918164352	11 a 5 4 9 a 6 5 5 5 5 5	11 1.5 3 10 8 6.5 5 1.5 6.5 9	11 19 10 78 4.5 2.5 3.1	18 9719 36 154 2	11 9.5 5 9.5 16 27 4 3	11 10 4 6 8 7 1 9 3 2 5
							Fler	ural stre	ngth ^b							
Al Bl ^o Bl ^o Ul Bl El El	2 10 9 7 3 8 1 5 6 1	301196.5 256.8 1	11 9 4 26 5 3 7 8 10 1	10 75 36 4 21 98 1	8 19 5 5 1 1 1 7 3 2	110953784621	11 19 96 78 35 4 21	11 9 10 86 7 3 5 4 2	6 4 5 38 11 7 10 9 1 2	8 + 5 3 6 H 7 12 9 1 2	116 8.5 3 10 4 5 5 7 2 1	8 9 1 3 7 2 5 10 6 4 1	11. 7069285431	17659389421	11 6 3 2 9 5 10 8 7 1	1954 2738 H6 91
								asticity	in flex	mep						
AL ME CL ME EL HL HL HL HL HL HL HL HL HL HL HL HL HL	8 10 11 7 3 2 4 5 6 9 1	11 10 8 9 4.5 3 1 7 4.5 6 2	11 97 34 5 28 6 10	11 8 4 5 6 2 1 9 7 19 3	11 7 9 5 3 6 2 8 3 5 10 1	1189634 27501	18 93 14 26 57 10 1	18973256401	10 76.35 11.49812	11 7 4 36 10 2 9 8 15	11 396 51 78 10 2	H61074238591	114 938 27560 101	11 7 3 9 2 8 4 6 10 1	11 6 8 4 5 1 3 9 7 10 2	11 6 7 3 5 2 8 9 10 1
Maximum deflection in flexure ^b]					
AL BU CL DL FL DL DL DL DL DL DL DL DL DL DL DL DL DL	11 6 10 8 4 5 1 2 7 3 9	7.5 7.5 92 1 3 4	11 5.5 8 7.5 2 1 3 4 6	11 4 96 98 2 1 3 5 7	10.5 6 8 9 5 10.5 10 4 2 1 7 3	11 5 10 96 8 1 4 3 7 2	11 10 8 4 39 25 6 1	116 10 54 98 1 37 2	10 8 5.5 7 9 11 12 34 5.5	10 96 71 11 235	11 7 9 8 4 10 3 1 26 5	11 2 10 9 7 4 5 1 6 8 3	17 10 598 31 2664	11 7 9 8 5 10 3 1 4 6 2	11 19 10 8 7 3 2 1 4 6 5	11 8 10 96 7 1 1 3 2 5

apata for tests other than the 2-year outdoor weathering and accelerated weathering by Method No. 6023 were taken from reference 1.

For changes in weight and dimensions the materials are rated according to the degree of change, the least change being denoted by a rating of 1. For the flexural strength and the flexural modulus of elasticity the materials are rated according to the retention of strength, the material with the greatest increase being rated 1 and that with the greatest decrease being rated 11.

For the maximum deflection in flexure the material with the greatest negative change is rated as 1 and that with the greatest positive change as 11.

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Positive change as il.

Method No. 6021, Federal Specification L-P-406a (reference 2).

Method No. 6023, Federal Specification L-P-406a (reference 2).

Specimens cut lengthwise.

Specimens cut crosswise.

TABLE IV. - CHANGES IN FLEXURAL STRENGTH, MODULUS OF ELASTICITY, AND MAXIMUM DEFLECTION IN FLEXURE OF PLASTICS DURING

OUTDOOR AND ACCELERATED WEATHERING TESTS

Material desig- nation	Initial strength (lb/sq in.), modulus (lb/sq in.), or deflection (mils)	Change during outdoor weathering test, 2 years (percent)	Changes durin weatheri (b 5 cycles	10 cycles									
		(a)	(percent)	(percent)									
	Flexural strength												
AL BL ^C CI DL EL FL HL LL KL	12,700 42,600 29,000 25,100 23,500 34,100 16,100 13,100 22,900 17,400 9,000	-13.4 -37.6 -39.3 -35.3 -24.3 -2.6 -20.5 -24.4 -24.9 -18.4 8.6	-8.7 -14.3 -13.1 -4.6 -4.7 -17.9 1.9 -3.0 -6.6	-25.9 -18.5 -15.9 -7.7 -4.3 -11.1 -15.5 -6.9 -8.3 -1.2 3.3									
Modulus of elasticity in flexure													
Al. BlC Bld Cl Dl El Fl Hl Tl Jl	1,170,000 3,363,000 1,845,000 2,567,000 1,920,000 1,810,000 706,000 652,000 1,238,000 1,121,000 986,000	-40.2 -34.8 -27.8 -29.4 -18.1 -7.1 2.0 -25.3 -18.2 -22.1 -1.9	-41.7 -16.3 -20.0 -13.5 -10.6 -14.4 -4.2 -17.5 -10.5 -22.0	-47.2 -18.9 -23.9 -16.0 -10.9 -13.6 -8.8 -17.9 -14.7 -25.3 13.8									
	Maximum deflection in flexure												
Al Blc Bld Cl Dl Bl Fl HL II JJ	24.0 26.4 31.0 27.4 21.5 45.7 72.7 68.2 65.2 41.2 21.0	41.7 -2.6 .0 .0 -10.2 5.0 -39.9 -40.2 -18.4 -13.8 6.2	43.3 11.4 21.9 24.1 8.8 43.5 7.2 -8.6 -8.9 14.8 -3.8	45.8 8.8 38.7 23.4 10.7 18.8 -8.2 3.7 -1.5 16.5 -4.8									

^aWashington, D. C.; specimens facing south on racks inclined at 45°. ^bMethod No. 6023, Federal Specification L-P-406a (reference 2). ^cSpecimens cut lengthwise. ^dSpecimens cut crosswise.